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## FEATURES

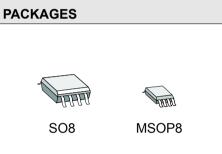
- Simple APC adjustment via an external resistor
- Continuous (CW) or pulsed operation of up to 300 kHz
- Laser diode current of up to 100 mA
- Adjustable watchdog for input signals
- Soft power-on and thermal protection
- Driver shutdown in case of overtemperature and undervoltage
- Operation at 2.7 to 6 V with two to four AA/AAA cells
- Protection against reverse polarity

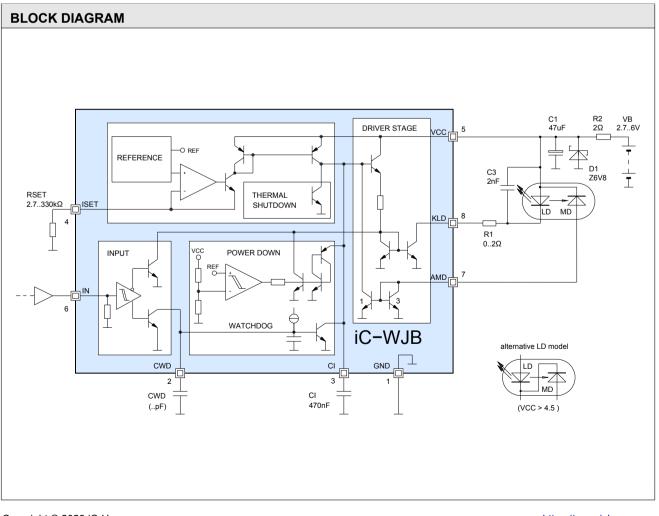


**APPLICATIONS** 

LD Pointers

Battery supplied LD modules







## DESCRIPTION

The iC-WJB device is a driver IC for laser diodes in continuous or pulsed operation of up to 300 kHz. The wide power supply range of 2.7 to 6 V and the integrated reverse battery protection allows for battery-operation with two to four AA/AAA cells.

The laser diode is activated via switching input IN. A control to the average value of the optical laser power (APC) and integrated protective functions ensure non-destructive operation of the sensitive semiconductor laser.

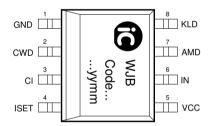
The IC contains protective diodes to prevent destruction due to ESD, a protective circuit to guard against overtemperature and undervoltage and a soft-start circuit to protect the laser diode when switching on the power supply. Short-term reversed battery connection destroys neither the IC nor the laser diode.

An external resistor at ISET is employed to adapt the APC to the laser diode being used. The capacitor at CI determines the recovery time constants and the starting time.

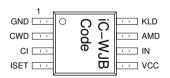
A watchdog circuit monitors the switching input IN. If IN remains low longer than preset by the capacitor at CWD, the capacitor of the APC is discharged at pin CI. This ensures that the current through the laser diode during the next high pulse at input IN is not impermissibly high.

## PACKAGING INFORMATION SO8, MSOP8 to JEDEC Standard

## PIN CONFIGURATION SO8



## **PIN CONFIGURATION MSOP8**



### PIN FUNCTIONS No. Name Function

- 1 GND Ground
- 2 CWD Capacitor for Watchdog
- 3 CI Capacitor for Power Control
- 4 ISET Reference Current Input
- 5 VCC +2.7 to +6 V Supply Voltage
- 6 IN Input
- 7 AMD Anode Monitor Diode
- 8 KLD Cathode Laser Diode



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## **ABSOLUTE MAXIMUM RATINGS**

Beyond these values damage may occur; device operation is not guaranteed.

Item	Symbol	Parameter	Conditions			Unit
No.				Min.	Max.	
G001	VCC	Supply Voltage VCC		-0.3	6.5	V
G002	VCC	Reverse Voltage at VCC	T < 10 s	-3		V
G003	I(VCC)	Current in VCC	T < 10 s	-500	50	mA
G004	I(CI)	Current in CI		-4	4	mA
G005	V(KLD)	Voltage at KLD	IN = Io	0	9	V
G006	I(KLD)	Current in KLD	IN = hi IN = lo	-4 -4	400 4	mA mA
G007	I(AMD)	Current in AMD		-6	6	mA
G008	I(IN)	Current in IN		-10	2	mA
G009	I(ISET)	Current in ISET		-2	2	mA
G010	I(CWD)	Current in CWD	IN = Io	-2	2	mA
G011	Vd()	ESD Susceptibility at CWD, CI, ISET, IN, AMD, KLD	HBM, 100 pF discharged through $1.5  k\Omega$		1	kV
G012	Tj	Junction Temperature		-40	150	°C
G013	Ts	Storage Temperature		-40	150	°C

## THERMAL DATA

Operating Conditions: VCC = 2.7...6 V

Item	Symbol	Parameter	Conditions				Unit
No.	-			Min.	Тур.	Max.	
T01	Та	Operating Ambient Temperature Range (extended temperature range on request)		-25		90	°C
T02	Rthja	Thermal Resistance Chip to Ambient	surface mounted on PCB, without special cooling			170	K/W



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## **ELECTRICAL CHARACTERISTICS**

ltem	Symbol	ns: VCC = 2.76 V, RSET = 2.72	Conditions				Unit
No.				Min.	Тур.	Max.	
Total	Device	1	,	0			
001	VCC	Permissible Supply Voltage Range		2.7		6	V
002	ldc(VCC)	Supply Current in VCC	RSET = $5 \text{ k}\Omega$ , IN = hi, Idc(KLD) = 40 mA	4	7	13	mA
003	I0(VCC)	Standby Supply Current in VCC	REST= 5 kΩ, IN = lo, Tj = 27 °C		5		mA
004	lav(VCC)	Supply Current in VCC (average value)	lpk(KLD) = 80 mA, f(IN) = 200 kHz ±20 %, twhi / twlo = 1		9	15	mA
005	tp(IN-KLD)	Delay Time Pulse Edge V(IN) to I(KLD)	IN(hi $\leftrightarrow$ lo), V(50 %) : I(50 %)	55		135	ns
006	Pcon	Power Consumption	VCC = 3 V, V(KLD) $\approx$ 0.6 V, RSET = 5 k $\Omega$ , ldc(KLD) = 40 mA		50		mW
007	Vc()hi	Clamp Voltage hi at VCC, IN, AMD, KLD, CI, CWD, ISET	l() = 2 mA, other pins open Tj = 27 °C	6.2	7.5	10	V V
Drive	r						
101	Vs(KLD)	Saturation Voltage at KLD	IN = hi, I(KLD) = 80 mA Tj = 27 °C		0.11	0.3	V V
102	Vs(KLD)	Saturation Voltage at KLD	IN = hi, I(KLD) = 100 mA			0.4	V
103	I0(KLD)	Leakage Current in KLD	IN = Io, V(KLD) = VCC			10	μA
104	V(AMD)	Voltage at AMD	I(AMD) = 1.5 mA Tj = 27 °C	0.4	0.84	1.0	V V
105	tr	Current Rise Time in KLD	Imax(KLD) = 2080 mA, Ip(): 10 $\rightarrow$ 90 % Tj = 27 °C		30	100	ns ns
106	tf	Current Fall Time in KLD	lmax(KLD) = 2080 mA, Ip(): 90 % $\rightarrow$ 10 % Tj = 27 °C		20	100	ns ns
107	CR1()	Current Ratio I(AMD)/I(ISET)	I(CI) = 0, closed control loop; RSET = 2.727 kΩ RSET = 27330 kΩ	2.4 2.4	3 3.6	3.8 5.4	
108	CR2()	Current Ratio I(AMD)/I(CI)	V(CI) = 12 V, ISET open	2.7	3	3.3	
109	TC1()	Temperature Coefficient of Current Ratio I(AMD)/I(ISET)	I(CI) = 0, closed control loop; RSET = 2.727 kΩ RSET = 27330 kΩ		0.01 -0.1	-0.25	%/°C %/°C
Input	IN	1	1	U			11
201	Vt()hi	Threshold hi		45		70	%VCC
202	Vt()lo	Threshold lo		40		65	%vcc
203	Vt()hys	Hysteresis	Tj = 27 °C	20	65		mV mV
204	Rin	Pull-Down Resistor	V(IN) = -0.3 VVCC Tj = 27 °C	4	10	16	kΩ kΩ
205	V0()	Open-loop Voltage	I(IN) = 0			0.1	V
Refer	ence und Th	ermal Shutdown		U			
301	V(ISET)	Voltage at ISET	Tj = 27 °C	1.16	1.22	1.28	V V
302	CR()	Current Ratio I(CI)/I(ISET)	V(CI) = 12 V, I(AMD) = 0	0.9	1	1.12	
303	RSET	Permissible Resistor at ISET (Control Set-up Range)		2.7		330	kΩ
304	Toff	Thermal Shutdown Threshold		125		150	°C
305	Thys	Thermal Shutdown Hysteresis		10		40	°C
Powe	r-Down and	-	1	U	L		0
401	VCCon	Turn-on Threshold VCC	Ti = 27 °C	2.4	2.6	2.7	V V
402	VCCoff	Undervoltage Threshold at VCC	Tj = 27 °C	2.3	2.5	2.63	VV
403	VCChys	Hysteresis	VCChys = VCCon – VCCoff	70	100	150	mV
404	Vs(CI)off	Saturation Voltage at CI with undervoltage	$I(CI) = 300 \mu\text{A},  \text{VCC} < \text{VCCoff}$	-		1.5	V



## **ELECTRICAL CHARACTERISTICS**

### Operating Conditions: VCC = 2.7...6 V, RSET = 2.7...27 kΩ, I(AMD) = 0.15...1.5 mA, Tj = -25...125 °C, unless otherwise noted.

Item	Symbol	Parameter	Conditions				Unit
No.				Min.	Тур.	Max.	
405	Vs(CI)wd	Saturation Voltage at CI with IN = Io	I(CI) = 300 μA, t(IN = Io) > tp <sup>(*)</sup>			1.5	V
406	lsc(CWD)	Pull-Up Current at CWD	V(CWD) = 0, IN = Io	2		15	μA
407	tpmin	Min. Activation Time for Watchdog	IN = lo, CWD open Tj = 27 °C	10	25		μs µs
408	Kwd <sup>(*)</sup>	Constant for Calculating the Watchdog Activation Time	IN = lo Tj = 27 °C	0.19	0.25	0.57	μs/pF μs/pF

 $^{(*)}$  tp = (C(CWD) \* Kwd) + tpmin (see Applications Information)



## **APPLICATIONS INFORMATION**

#### Laser Power Adjustment

The iC-WJB device can be adapted to CW laser diodes of up to 40 mW. When the supply voltage is higher than approx. 4.5 V, LD models in common cathode configuration can be used.

The pin ISET is used for the adjustment to the sensitivity of the monitor diode and to set the desired optical laser power. The setpoint for the averaging control of the monitor diode current is pre-set at this pin.

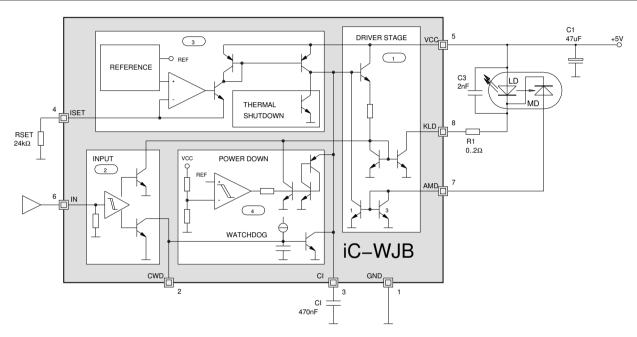


Figure 1: Circuit diagram for LD models with a common cathode

To calculate the current required at ISET, the average optical laser power is to determine:

$$P_{av} = P_{peak} * \frac{t_{whi}}{T}$$

with peak value  $P_{peak}$  and pulse/period duration  $t_{whi}/T$ .

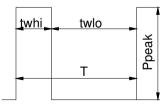


Figure 2: Duty cycle

#### Example for CW operation

 $P_{cw}$  = 1 mW (pin IN at VCC, pin CWD open), laser diode maximum optical output of 3 mW, monitor diode with 0.75 mA at 3 mW.

At  $P_{av} = P_{cw} = 1 \text{ mW}$ , the monitor diode current is 0.25 mA and RSET is calculated to:

$$RSET = \frac{CR1 * V(ISET)}{I_{av}(AMD)} = \frac{3 * 1.22 V}{0.25 mA} = 14.64 k\Omega$$

with Electrical Characteristics No. 301 for V(ISET) and No. 107 for current ratio CR1.

#### Example for pulse operation

Pulse duty factor  $t_{whi}/T$  set to 20 % at  $P_{peak} = 3 \text{ mW}$ , laser diode as above with maximum optical output of 3 mW, monitor diode with 0.75 mA at 3 mW.

The average optical power is set to 0.6 mW by the pulse duty factor; the average monitor diode current  $I_{AV}$  is then 0.15 mA. The resistor RSET is calculated to:

$$RSET = \frac{CR1 * V(ISET)}{I_{av}(AMD)} = \frac{3 * 1.22 V}{0.15 mA} = 24.4 k\Omega$$

with the Electrical Characteristics No. 301 for V(ISET) and No. 108 for current ratio CR1.

#### Averaging control (APC)

The control of the average optical laser power requires a capacitor at pin CI. This capacitor is used for averaging and must be adjusted to the selected pulse repetition frequency and the charging current preset with RSET. The ratios are linear in both cases, i.e. the capacitor CI must be increased in size proportionally as the pulse repetition frequency slows or the current from ISET increases:

$$CI \geq \frac{440 * I(ISET)}{f * V(ISET)} = \frac{440}{f * RSET}$$

#### Example

Pulse repetition frequency 100 kHz, RSET =  $10 \text{ k}\Omega$ : CI = 440 nF, chosen 470 nF.

Otherwise the charging of the capacitor CI during the pulse pauses (with I(ISET) = 1.22 V / RSET) will create an excessive average value potential and may destroy the laser diode during the next pulse. The capacitor CI is correctly dimensioned when the current through the laser diode and the optical output signal do not show any overshots following the rising edge.

In steady-state condition and for a pulse duty factor of 50% (pulse / pause = 1:1), wave forms as shown in Figure 3.

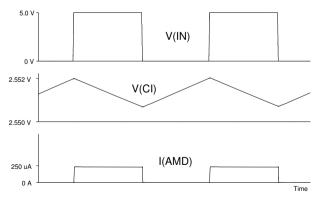


Figure 3: Steady-state APC, f(IN) = 100 kHz (1:1), CI = 470 nF, RSET = 10 k $\Omega$ 

Figure 4 shows the corresponding signals for a pulse duty factor of 20%. The influence of the pulse duty factor on the peak value of the monitor current proportional to the laser current is apparent. The average kept constant by the control (RSET unchanged) means a peak value increased by the factor 2.5. The pulse duty factor for which RSET was dimensioned should therefore be kept constant if possible.



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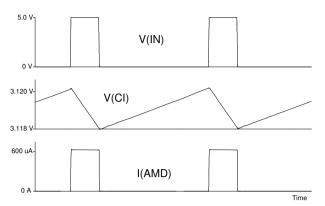


Figure 4: Steady-state APC, f(IN) = 100 kHz (1:4), CI = 470 nF, RSET = 10 k $\Omega$ 

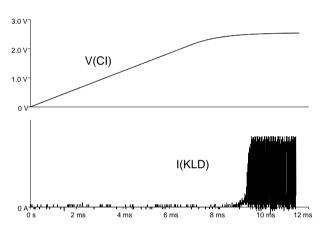


Figure 5: Turn-on behaviour, f(IN) = 100 kHz (1:1), CI = 470 nF, RSET = 10 k $\Omega$ 

#### Turn-on and turn-off behaviour

Capacitor CI also determines the starting time from switching on the supply voltage VCC to steady-state laser pulse operation or after a discharge of CI by the watchdog. The following applies to estimating the starting time (Figure 5):

$$T_{on} \approx \frac{1.7 \text{ V} * \text{CI}}{\text{I(ISET)}} = \frac{1.7 \text{ V} * \text{CI} * \text{RSET}}{1.22 \text{ V}}$$

#### Example

CI = 470 nF, RSET = 10 k\Omega:  $T_{on}\approx 6.5\,ms$ 

Figure 6 shows a detailed view of the start of laser operation; Figure 7 shows the shut-down behaviour. The decline in the voltage at CI and the absence of the laser pulses indicate that the undervoltage detector is active.





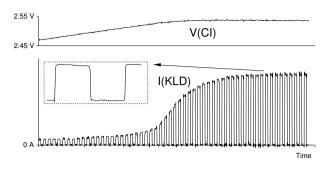


Figure 6: Turn-on behaviour, detailed view f(IN) =100 kHz (1:1), CI = 470 nF, RSET = 10 k $\Omega$ 

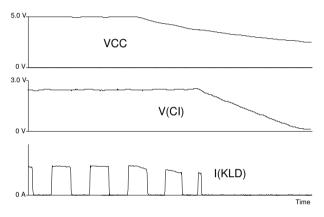


Figure 7: Turn-off behaviour, f(IN) = 100 kHz (1:1), CI = 470 nF, RSET = 10 k $\Omega$ 

#### Watchdog

The watchdog ensures that the capacitor CI is discharged during protracted pulses at IN. During the pulse pauses the voltage at CI increases by  $\Delta V$  (Figure 3).

$$\Delta V = \frac{l(ISET) * t_{wlo}}{CI}$$

The discharge of capacitor CI by the watchdog protects the laser diode from being destroyed by an excessive turn-on current during the next pulse.

The capacitor CWD should be dimensioned such that the response time  $t_p$  of the watchdog is slightly longer than the pulse pause  $t_{wlo}$  of the input signal. As a result, the watchdog is just short of being activated.

For response times t<sub>p</sub> longer than t<sub>pmin</sub> applies:

$$CWD = \frac{t_p - t_{pmin}}{K_{wd}}$$

with  $t_{\text{pmin}}$  and  $K_{\text{wd}}$  from Electrical Characteristics No. 407, 408.

Figure 8 shows the signals during normal operation, without the watchdog being activated. The potential at

CWD rises during pulse pauses but does not reach the watchdog activation threshold.

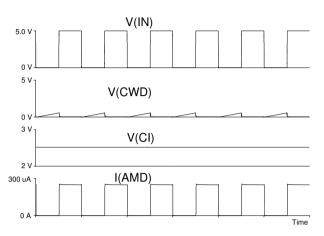


Figure 8: Watchdog, CWD open, f(IN) = 100 kHz(1:1), CI = 470 nF, RSET = 10 k $\Omega$ 

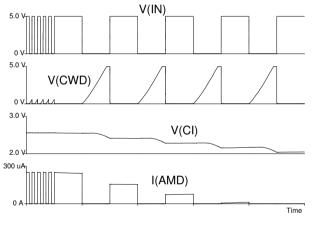


Figure 9: Watchdog, CWD open, f(IN) = 100 kHz  $\rightarrow$  10 kHz (1:1), CI = 470 nF, RSET = 10 k $\Omega$ 

Figure 9 shows the watchdog behaviour when the input frequency is reduced from 100 kHz to 10 kHz. The pulse pauses are longer than the watchdog's response time. The watchdog begins to discharge the capacitor CI current limited. The remaining charge time during the pulse pauses before further watchdog intervention is not sufficient to maintain the initial potential at CI. The potential is thus gradually reduced until it reaches the saturation voltage Vs(CI)<sub>wd</sub> (Electrical Characteristics No. 405).

The watchdog therefore protects the laser diode from destruction when the input signal change in such a manner that the capacitor CI is not longer adequate for averaging.

Furthermore, the introduction of the watchdog permits long pulse pauses and activation of the laser diode with pulse packets.



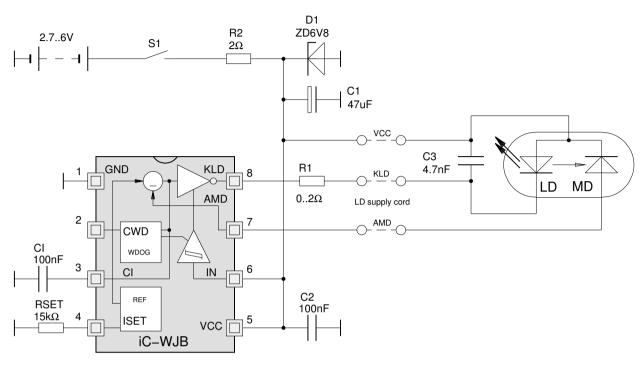


Figure 10: CW operation via cable plus protective circuitry

#### **CW** Operation

In case of CW operation, the input IN can be connected to the power supply VCC. The pin CWD may be left open, because the capacitor for the watchdog is not necessary. The capacitor CI for the averaging control can be reduced to 100 nF.

#### Operation of laser diode via cable

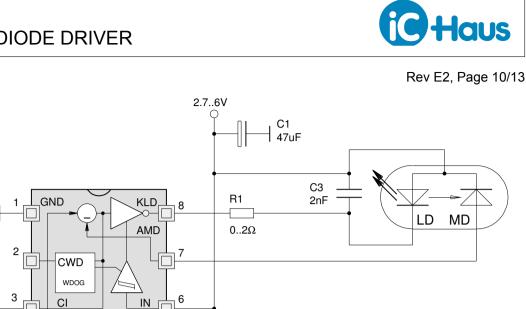
It is recommended to connect a capacitor of 1 to 10 nF across the laser diode in order to protect the laser diode against destruction due to ESD or transients. This capacitor should be placed close to the laser diode and not at the beginning of the LD supply line.

An approx. 2  $\Omega$  series resistor at pin KLD reduces the IC power consumption and damps possible resonances

of the load circuit caused by the inductive LD supply line. This resistor is useful for many applications, also for those which do not operate via cable.

On a PCB the forward path VCC to the laser diode should be arranged in parallel with the return path to KLD even when the line is only a few centimeters in length.

Additional protective components for clipping of strong positive and negative spikes can be useful, in particular when contact bouncing occurs in an inductive accumulator power supply line. Elements which come into guestion here are D1 and R1 as in Figure 10.



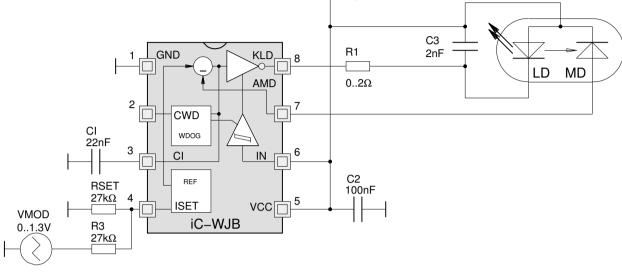


Figure 11: Analogue modulation during CW operation

## Analogue modulation during CW operation

The modulation cut-off frequency is determined by the capacitor CI as well as by the operating point set with the resistor RSET. With CI = 100 nF and RSET = R3 =  $15 \text{ k}\Omega$  the cut-off frequency is approx. 30 kHz, with CI = 22 nF and the same resitor value of about 150 kHz.

The laser power can also be modulated by adapting a current source, e.g. by using an operational amplifier with a current output (OTA). To limit the current at pin ISET while turning on the power supply for the OTA circuitry, however, RSET should be connected to the OTA output (instead of to GND). The maximum current possible at ISET must be taken into consideration when dimensioning the capacitor CI.

## PC board layout

The ground connections of the external components CI, CWD and RSET have to be directly connected at the IC with the GND terminal.



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## **DEMO BOARD**

For the devices iC-WJ/WJZ/WJB a Demo Board is available for test purpose. The following figures show the schematic diagram and the component side of the test PCB.

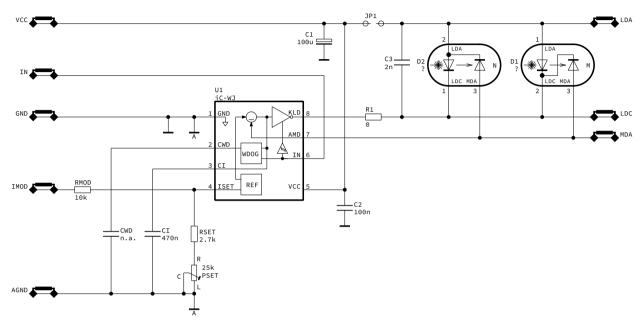


Figure 12: Schematic diagram of the Demo Board

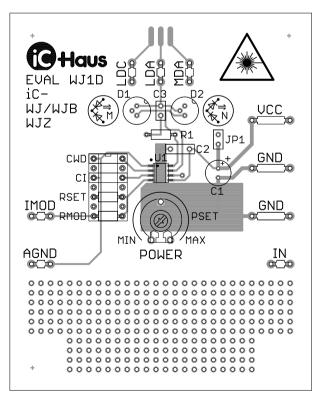


Figure 13: Demo Board (components side)



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### **REVISION HISTORY**

ſ	Rel.	Rel. Date <sup>*</sup>	Chapter	Modification	Page
	E2	2023-09-19	DEMO BOARD	New PCB	11

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## **ORDERING INFORMATION**

Туре	Package	Order Designation
iC-WJB iC-WJB iC-WJB	MSOP8	iC-WJB SO8 iC-WJB MSOP8 iC-WJB EVAL WJ1D

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